| Q 1 |  | mark |  | sub |
| :---: | :---: | :---: | :---: | :---: |
| (i) | $\begin{aligned} & \text { before } \\ & \frac{v_{1}-v_{2}}{0-10}=-0.8 \\ & v_{1}=0.3 \text { so } V_{1}=0.3 \\ & v_{2}=-7.7 \text { so } V_{2}=7.7 \mathrm{~m} \mathrm{~s}^{-1} \end{aligned}$ <br> in opposite to original direction | $\begin{aligned} & \text { M1 } \\ & \text { A1 } \\ & \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { F1 } \end{aligned}$ | PCLM and two terms on RHS <br> All correct. Any form. <br> NEL <br> Any form <br> Speed. Accept $\pm$. <br> Must be correct interpretation of clear working | 7 |
| $\overline{\text { (ii) }}$ (A) | $\begin{aligned} & 10 \times 0.5=30 V \\ & \text { so } V=\frac{1}{6} \end{aligned}$ | $\begin{aligned} & \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \end{aligned}$ | PCLM and coalescence <br> All correct. Any form. <br> Clearly shown. Accept decimal equivalence. Accept no direction. | 3 |
| (B) | Same velocity <br> No force on sledge in direction of motion | $\begin{aligned} & \text { E1 } \\ & \text { E1 } \end{aligned}$ | Accept speed | 2 |
| (iii) | $\begin{aligned} & 2 \times 40=0.5 u+39.5 V \\ & u-V=10 \\ & \text { Hence } V=1.875 \end{aligned}$ | B1 <br> M1 <br> A1 <br> B1 <br> A1 | PCLM, masses correct <br> Any form May be seen on the diagram. Accept no reference to direction. | 5 |
|  |  | 17 |  |  |


| Q 2 |  | mark | comment | sub |
| :---: | :---: | :---: | :---: | :---: |
| (i) | $\begin{align*} & X=R \cos 30  \tag{1}\\ & Y+R \sin 30=L \tag{2} \end{align*}$ | B1 <br> M1 A1 | Attempt at resolution | 3 |
| (ii) | ac moments about A $\quad R-2 L=0$ <br> Subst in (1) and (2) $\begin{aligned} & X=2 L \frac{\sqrt{3}}{2} \text { so } X=\sqrt{3} L \\ & Y+2 L \times \frac{1}{2}=L \text { so } Y+L=L \text { and } Y=0 \end{aligned}$ | B1 <br> M1 <br> E1 <br> E1 | Subst their $R=2 L$ into their (1) or (2) <br> Clearly shown <br> Clearly shown | 4 |
| (iii) | (Below all are taken as tensions e. g. $T_{\mathrm{AB}}$ in AB) | $\begin{aligned} & \text { B1 } \\ & \text { B1 } \end{aligned}$ | Attempt at all forces (allow one omitted) Correct. Accept internal forces set as tensions or thrusts or a mix | 2 |
| (iv) | $\begin{aligned} & \downarrow \mathrm{A} \quad T_{\mathrm{AD}} \cos 30(-Y)=0 \\ & \text { so } T_{\mathrm{AD}}=0 \end{aligned}$ | $\begin{aligned} & \text { M1 } \\ & \text { E1 } \end{aligned}$ | Vert equilibrium at A attempted. $Y=0$ need not be explicit | 2 |
| (v) | Consider the equilibrium at pin-joints $\begin{align*} & \mathrm{A} \rightarrow \quad T_{\mathrm{AB}}-X=0 \text { so } T_{\mathrm{AB}}=\sqrt{3} L  \tag{T}\\ & \mathrm{C} \downarrow \quad L+T_{\mathrm{CE}} \cos 30=0 \\ & \text { so } T_{\mathrm{CE}}=\frac{-2 L}{\sqrt{3}} \text { so } \frac{2 \mathrm{~L}}{\sqrt{3}}\left(=\frac{2 L \sqrt{3}}{3}\right)  \tag{C}\\ & \mathrm{C} \leftarrow \quad T_{\mathrm{BC}}+T_{\mathrm{CE}} \cos 60=0 \\ & \text { so } T_{\mathrm{BC}}=-\left(-\frac{2 \sqrt{3} L}{3}\right) \times \frac{1}{2}=\frac{\sqrt{3} L}{3} \tag{T} \end{align*}$ | M1 <br> B1 <br> B1 <br> B1 <br> B1 <br> B1 <br> F1 | At least one relevant equilib attempted <br> (T) not required <br> Or equiv from their diagram <br> Accept any form following from their equation. (C) not required. <br> Or equiv from their diagram <br> FT their $T_{\text {CE }}$ or equiv but do not condone inconsistent signs even if right answer obtained. (T) not required. <br> T and C consistent with their answers and their diagram | 7 |
| (vi) | $\downarrow \mathrm{B} \quad T_{\mathrm{BD}} \cos 30+T_{\mathrm{BE}} \cos 30=0$ <br> so $T_{\mathrm{BD}}=-T_{\mathrm{BE}}$ so mag equal and opp sense | $\begin{aligned} & \text { M1 } \\ & \text { E1 } \end{aligned}$ | Resolve vert at B <br> A statement required | 2 |
|  |  | 20 |  |  |


| Q 3 |  | mark |  | sub |
| :---: | :---: | :---: | :---: | :---: |
| (i) | (10, 2, 2.5) | B1 |  | 1 |
| (ii) | $\begin{aligned} & \text { By symmetry } \\ & \bar{x}=10, \\ & \bar{y}=2 \\ & (240+80) \bar{z}=80 \times 0+240 \times 2.5 \\ & \text { so } \bar{z}=1.875 \end{aligned}$ | $\begin{aligned} & \text { B1 } \\ & \text { B1 } \\ & \text { B1 } \\ & \text { M1 } \\ & \text { A1 } \end{aligned}$ | Total mass correct Method for c.m. Clearly shown | 5 |
| (iii) | $\begin{aligned} & \bar{x}=10 \text { by symmetry } \\ & (320+80)\left(\begin{array}{c} \bar{x} \\ \bar{y} \\ \bar{z} \end{array}\right)=320\left(\begin{array}{c} 10 \\ 2 \\ 1.875 \end{array}\right)+80\left(\begin{array}{c} 10 \\ 4 \\ 3 \end{array}\right) \\ & \bar{y}=2.4 \\ & \bar{z}=2.1 \end{aligned}$ | E1 <br> M1 <br> B1 <br> B1 <br> E1 <br> E1 | Could be derived <br> Method for c.m. <br> $y$ coord c.m. of lid z coord c.m. of lid shown shown | 6 |
| (iv) | c.w moments about X $\begin{aligned} & 40 \times 0.024 \cos 30-40 \times 0.021 \sin 30 \\ & =0.41138 \ldots \text { so } 0.411 \mathrm{~N} \mathrm{~m}(3 \mathrm{~s} . \mathrm{f} .) \end{aligned}$ | B1 <br> B1 <br> B1 <br> E1 | Award for correct use of dimensions 2.1 and 2.4 or equivalent <br> $1^{\text {st }}$ term o.e. (allow use of 2.4 and 2.1) <br> $2^{\text {nd }}$ term o.e. (allow use of 2.4 and 2.1) <br> Shown <br> [Perpendicular method: M1 Complete method: <br> A1 Correct lengths and angles <br> E1 Shown] | 4 |
| (v) | $\begin{aligned} & 0.41138 \ldots-0.05 P=0 \\ & P=8.22768 \ldots \ldots \text { so } 8.23(3 \mathrm{s.} \text { f. }) \end{aligned}$ | M1 <br> A1 | Allow use of 5 <br> Allow if cm used consistently | 2 |
|  |  | 18 |  |  |


| Q 4 |  | mark |  | sub |
| :---: | :---: | :---: | :---: | :---: |
| (i) | $\begin{aligned} & F_{\max }=\mu R \\ & R=2 g \cos 30 \\ & \text { so } F_{\max }=0.75 \times 2 \times 9.8 \times \cos 30=12.730 \ldots \\ & \text { so } 12.7 \mathrm{~N}(3 \text { s. f. }) \end{aligned}$ <br> either <br> Weight cpt down plane is $2 g \sin 30=9.8 \mathrm{~N}$ so no as $9.8<12.7$ <br> or <br> Slides if $\mu<\tan 30$ <br> But $0.75>0.577 \ldots$ so no | M1 <br> B1 <br> A1 <br> B1 <br> E1 <br> B1 <br> E1 | Must have attempt at $R$ with mg resolved <br> [Award $2 / 3$ retrospectively for limiting friction seen below] <br> The inequality must be properly justified <br> The inequality must be properly justified | 5 |
| (ii) <br> (A) | Increase in GPE is $2 \times 9.8 \times(6+4 \sin 30)=156.8 \mathrm{~J}$ | $\begin{aligned} & \text { M1 } \\ & \text { B1 } \\ & \text { A1 } \end{aligned}$ | Use of $m g h$ $6+4 \sin 30$ | 3 |
| (B) | WD against friction is $4 \times 0.75 \times 2 \times 9.8 \times \cos 30=50.9222 \ldots \mathrm{~J}$ | $\begin{aligned} & \text { M1 } \\ & \text { A1 } \end{aligned}$ | Use of WD = Fd | 2 |
| (C) | Power is $10 \times(156.8+50.9222 \ldots) / 60$ $=34.620 \ldots \text { so } 34.6 \mathrm{~W} \text { (3 s. f.) }$ | M1 <br> A1 | Use $P=\mathrm{WD} / \mathrm{t}$ | 2 |
| (iii) | $\begin{aligned} & 0.5 \times 2 \times 9^{2} \\ & =2 \times 9.8 \times(6+x \sin 30) \\ & +0.5 \times 2 \times 4^{2} \\ & -90 \\ & \text { so } x=3.8163 \ldots \text { so } 3.82 \text { ( } 3 \text { s. f.) } \end{aligned}$ | M1 <br> B1 <br> A1 <br> A1 <br> A1 | Equating KE to GPE and WD term. Allow sign errors and one KE term omitted. Allow 'old' friction as well. <br> Both KE terms. Allow wrong signs. <br> All correct but allow sign errors <br> All correct, including signs. <br> cao | 5 |
|  |  | 17 |  |  |

